

ASSIGNMENT 6

CHE 3473

Solution

#Problem 1:

9.4

We have the following properties for a mixture for mixing at constant T and P :

$$U(T, P, \underline{x}) = \sum N_i \underline{U}_i(T, P)$$

$$V(T, P, \underline{x}) = \sum N_i \underline{V}_i(T, P)$$

$$S(T, P, \underline{x}) = \sum N_i \underline{S}_i(T, P) - R \sum N_i \ln x_i$$

$$\text{and } \underline{S}_i = \underline{S}_i^0 + C_{V,i} \ln \frac{\underline{U}_i}{\underline{U}_i^0} + R \ln \frac{\underline{V}_i}{\underline{V}_i^0}$$

$\underline{S}_i^0, \underline{U}_i^0, \underline{V}_i^0$ are at some reference state.

(a) Find $\bar{V}_i, \bar{U}_i, \bar{S}_i$ and \bar{G}_i in terms of $\underline{S}_i^0, \underline{U}_i^0, \underline{V}_i^0, C_{V,i}, R, T,$ and \underline{P} . Need $\underline{U}_i, \underline{V}_i$.

We know $d\underline{U} = Td\underline{S} - Pd\underline{V} \rightarrow \left. \frac{\partial \underline{S}}{\partial \underline{U}} \right|_{\underline{V}} = \frac{1}{T}; \left. \frac{\partial \underline{S}}{\partial \underline{V}} \right|_{\underline{U}} = \frac{P}{T}$ and $\underline{S}_i = \underline{S}_i^0 + C_{V,i} \ln \frac{\underline{U}_i}{\underline{U}_i^0} + R \ln \frac{\underline{V}_i}{\underline{V}_i^0}$ for

pure component i .

$$\left. \frac{\partial \underline{S}}{\partial \underline{U}} \right|_{\underline{V}} = \frac{1}{T} = C_{V,i} \frac{1}{\underline{U}_i} \rightarrow \underline{U}_i = C_{V,i} T$$

$$\left. \frac{\partial \underline{S}}{\partial \underline{V}} \right|_{\underline{U}} = R \frac{1}{\underline{V}_i} \text{ and } \left. \frac{\partial \underline{S}}{\partial \underline{V}} \right|_{\underline{U}} \cdot \left. \frac{\partial \underline{U}}{\partial \underline{S}} \right|_{\underline{V}} \cdot \left. \frac{\partial \underline{V}}{\partial \underline{U}} \right|_{\underline{S}} = -1$$

$$\left. \frac{\partial \underline{U}}{\partial \underline{S}} \right|_{\underline{V}} = T \left. \frac{\partial \underline{V}}{\partial \underline{U}} \right|_{\underline{S}} = -\frac{1}{P} \Rightarrow \left. \frac{\partial \underline{S}}{\partial \underline{V}} \right|_{\underline{U}} = T \cdot \frac{-1}{P} = -1 \rightarrow \left. \frac{\partial \underline{S}}{\partial \underline{V}} \right|_{\underline{U}} = \frac{R}{\underline{V}_i} = \frac{P}{T}$$

$$\Rightarrow \underline{V}_i = \frac{RT}{P}$$

$$\text{So } \bar{U}_i = \left. \frac{\partial U}{\partial N_i} \right|_{T,P,N_{j \neq i}} = \frac{\partial}{\partial N_i} \sum N_i C_{V,i} T = C_{V,i} T = \underline{U}_i$$

$$\bar{U}_i = C_{V,i} T$$

$$\bar{V}_i = \left. \frac{\partial V}{\partial N_i} \right|_{T,P,N_{j \neq i}} = \frac{\partial}{\partial N_i} \sum N_i \underline{V}_i = \frac{RT}{P} = \underline{V}_i = \bar{V}_i$$

$$\bar{S}_i = \left. \frac{\partial S}{\partial N_i} \right|_{T,P,N_{j \neq i}} = \frac{\partial}{\partial N_i} \left(\sum N_i \underline{S}_i(T, P) - R \sum N_i \ln x_i \right) = \underline{S}_i - R \ln x_i$$

$$\bar{S}_i = \underline{S}_i^0 + C_{v,i} \ln \frac{C_{v,i} T}{\underline{U}_i^0} + R \ln \frac{RT}{P \underline{V}_i^0} - R \ln x_i$$

$$\bar{G}_i = \left. \frac{\partial G}{\partial N_i} \right|_{T,P,N_{j \neq i}} = \frac{\partial}{\partial N_i} (H - TS)|_{T,P,N_{j \neq i}} = \frac{\partial}{\partial N_i} (U + PV - TS)|_{T,P,N_{j \neq i}}$$

$$\begin{aligned} \bar{G}_i &= \bar{U}_i + P\bar{V}_i - T \left. \frac{\partial S}{\partial N_i} \right|_{T,P,N_{j \neq i}} = \bar{U}_i + P\bar{V}_i - T\bar{S}_i \\ &= C_{v,i}T + RT - T(\underline{S}_i^o + C_{v,i} \ln \frac{C_{v,i}T}{\underline{U}_i^o} + R \ln \frac{RT}{P\underline{V}_i^o} - R \ln x_i) \end{aligned}$$

b)

$$V = \sum N_i \underline{V}_i = \sum N_i \frac{RT}{P} = \frac{NRT}{P}$$

$$U = \sum N_i \underline{U}_i = \sum N_i C_{v,i}T$$

c)

$$H = U + PV = \sum N_i \underline{U}_i + P \sum N_i \underline{V}_i = \sum N_i (\underline{U}_i + P\underline{V}_i) = \sum N_i \underline{H}_i$$

$$\begin{aligned} A &= U - TS = \sum N_i \underline{U}_i - T \left(\sum N_i \underline{S}_i(T, P) - R \sum N_i \ln x_i \right) \\ &= \sum N_i (\underline{U}_i - T\underline{S}_i + RT \ln x_i) = \sum N_i \underline{A}_i + RT \sum N_i \ln x_i \end{aligned}$$

$$\begin{aligned} G &= H - TS = \sum N_i \underline{H}_i - T \left(\sum N_i \underline{S}_i(T, P) - R \sum N_i \ln x_i \right) \\ &= \sum N_i (\underline{H}_i - T\underline{S}_i) + RT \sum N_i \ln x_i = \sum N_i \underline{G}_i + RT \sum N_i \ln x_i \end{aligned}$$

#Problem 2:
9.6

As a preliminary note that, from Eqns. (6.4-27 and 28)

$$\underline{H}(T, P) - \underline{H}^{\text{IG}}(T, P) = RT(Z - 1) + \int_{\underline{V}=\infty}^{\underline{V}=ZRT/P} \left[T \left(\frac{\partial P}{\partial T} \right)_{\underline{V}} - P \right] d\underline{V}$$

and

$$\underline{S}(T, P) - \underline{S}^{\text{IG}}(T, P) = R \ln Z + \int_{\underline{V}=\infty}^{\underline{V}=ZRT/P} \left[\left(\frac{\partial P}{\partial T} \right)_{\underline{V}} - \frac{R}{\underline{V}} \right] d\underline{V}$$

vdw E.O.S. $P = \frac{RT}{\underline{V}-b} - \frac{a}{\underline{V}^2}$ so

$$\begin{aligned} \left(\frac{\partial P}{\partial T} \right)_{\underline{V}} &= \frac{R}{\underline{V}-b}; \quad T \left(\frac{\partial P}{\partial T} \right)_{\underline{V}} - P = \frac{RT}{\underline{V}-b} - \frac{RT}{(\underline{V}-b)} + \frac{a}{\underline{V}^2} = \frac{a}{\underline{V}^2} \\ \left(\frac{\partial P}{\partial T} \right)_{\underline{V}} - \frac{R}{\underline{V}} &= \frac{R}{(\underline{V}-b)} - \frac{R}{\underline{V}}; \end{aligned}$$

$$\Rightarrow \underline{H}(T, P) - \underline{H}^{\text{IG}}(T, P) = RT(Z - 1) + \int_{\underline{V}=\infty}^{\underline{V}=ZRT/P} \frac{a}{\underline{V}^2} d\underline{V} = RT(Z - 1) - \frac{a}{\underline{V}} = RT(Z - 1) - \frac{RTA}{Z}$$

and

$$\begin{aligned} \underline{S}(T, P) - \underline{S}^{\text{IG}}(T, P) &= R \ln Z + \int_{\underline{V}=\infty}^{\underline{V}=ZRT/P} \left[\frac{R}{\underline{V}-b} - \frac{R}{\underline{V}} \right] d\underline{V} \\ &= R \ln Z + R \ln \frac{(\underline{V}-b)}{\underline{V}} \Big|_{\underline{V}=\infty}^{ZRT/P} = R \ln(Z - B) \end{aligned}$$

Now on to solution of problem.

$$(a) \underline{V}^{\text{ex}} = \underline{V}_{\text{max}} - \sum x_i \underline{V}_i = \frac{RT}{P} (Z_{\text{max}} - \sum x_i Z_i) = \Delta_{\text{max}} \underline{V}$$

Z_{max} = compressibility of mixture at T and P

Z_i = compressibility of pure fluid i at T and P

Will leave answer to this part in this form since the analytic expression for Z_i and Z_{max} (solution to cubic) is messy. Though it can be analytically and symbolically with a computer algebra program such as Mathcad, Mathematica, Maple, etc.)

$$(b) \underline{H}^{\text{ex}} = \underline{H}_{\text{max}} - \sum x_i \underline{H}_i = \frac{RT}{Z_{\text{max}} - 1} - \frac{RTA_{\text{max}}}{Z_{\text{max}}} - \sum_i x_i \left[RT(Z_i - 1) - \frac{RTA_i}{Z_{\text{max}}} \right]$$

$$\begin{aligned}
&= RT(Z_{\text{mix}} - \sum x_i Z_i) + \sum RT \left(\frac{x_i A_i}{Z_i} \right) - \frac{RT A_{\text{mix}}}{Z_{\text{mix}}} \\
&= RT(Z_{\text{mix}} - \sum x_i Z_i) + RT \left(\sum \frac{x_i A_i}{Z_i} - \frac{A_{\text{mix}}}{Z_{\text{mix}}} \right) \\
\underline{U}^{\text{ex}} &= (H_{\text{mix}} - PV_{\text{mix}}) - \sum x_i (H_i - PV_i) \\
&= (H_{\text{mix}} - \sum x_i H_i) - P(V_{\text{mix}} - \sum x_i V_i) \\
&= RT(Z_{\text{mix}} - \sum x_i Z_i) + RT \left(\sum \frac{x_i A_i}{Z_i} - \frac{A_{\text{mix}}}{Z_{\text{mix}}} \right) - RT(Z_{\text{mix}} - \sum x_i Z_i) \\
&= +RT \left(\sum \frac{x_i A_i}{Z_i} - \frac{A_{\text{mix}}}{Z_{\text{mix}}} \right)
\end{aligned}$$

$$\begin{aligned}
\text{(c) } \underline{S}_{\text{mix}} - \sum x_i S_i - R \sum x_i \ln x_i \\
&= \underline{S}^{\text{ex}} \\
&= P \ln(Z_{\text{mix}} - B_{\text{mix}}) - R \left[\sum x_i \ln(Z_i - B_i) - R \sum x_i \ln x_i \right] \\
&= R \ln(Z_{\text{mix}} - B_{\text{mix}}) - R \sum x_i [\ln(Z_i - B_i) + \ln x_i] \\
&= R \ln(Z_{\text{mix}} - B_{\text{mix}}) - R \left[\sum x_i \ln x_i (Z_i - B_i) \right] \\
&= R \ln \frac{Z_{\text{mix}} - B_{\text{mix}}}{\prod_i (Z_i - B_i)^{x_i}}
\end{aligned}$$

$$\begin{aligned}
\text{(d) } \underline{G}^{\text{ex}} &= \underline{H}^{\text{ex}} - T \underline{S}^{\text{ex}} = RT(Z_{\text{mix}} - \sum x_i Z_i) + RT \left(\sum \frac{x_i A_i}{Z_i} - \frac{A_{\text{mix}}}{Z_{\text{mix}}} \right) \\
&\quad - RT \ln \frac{Z_{\text{mix}} - B_{\text{mix}}}{\prod_i (Z_i - B_i)^{x_i}} \\
\underline{A}^{\text{ex}} &= \underline{U}^{\text{ex}} - T \underline{S}^{\text{ex}} = +RT \left(\sum \frac{x_i A_i}{Z_i} - \frac{A_{\text{mix}}}{Z_{\text{mix}}} \right) - RT \ln \frac{Z_{\text{mix}} - B_{\text{mix}}}{\prod_i (Z_i - B_i)^{x_i}}
\end{aligned}$$

#Problem 3:
9.22

- 2 (a) The two-constant Redlich-Kister expansion, which leads to the two-constant Margules equation is

$$\underline{G}^{\text{ex}} = x_1 x_2 \{A + B(x_1 - x_2)\}$$

Thus

$$\frac{\underline{G}^{\text{ex}}}{x_1 x_2} = A + B(2x_1 - 1) \quad (1)$$

which is a linear function of x .

The form of the Wohl Equation which leads to the van Laar Equation is

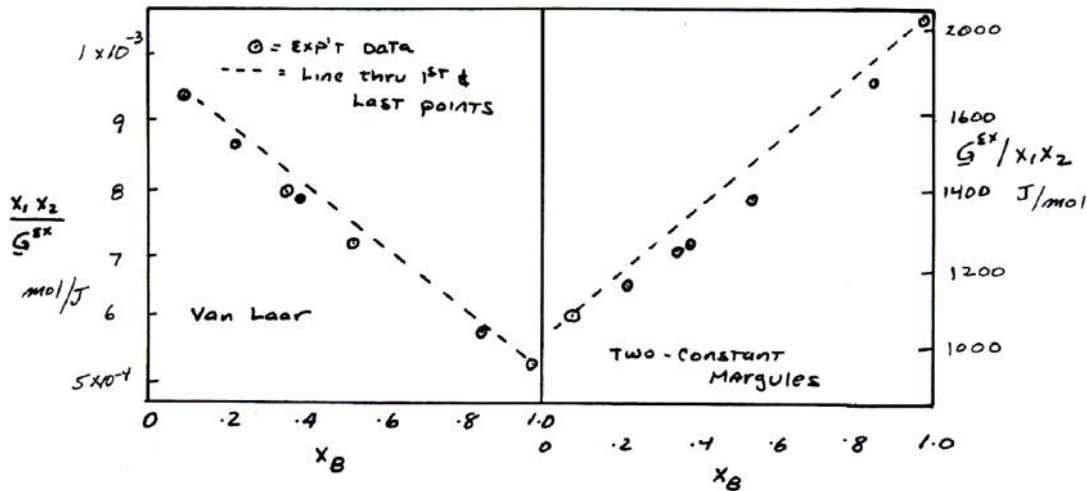
$$\underline{G}^{\text{ex}} = \frac{2RTa_{12}x_1q_1x_2q_2}{x_1q_1 + x_2q_2}$$

which can be rearranged to

$$\frac{x_1 x_2}{\underline{G}^{\text{ex}}} = \frac{x_1 q_1 + (1 - x_1) q_2}{2RT a_{12} q_1 q_2} \quad (2)$$

which is also a linear function of x . Equations (1) and (2) provide the justification for the procedure.

- (b) The figure below is the required plot. Clearly, neither equation is an accurate fit of the data. [The 2-constant Wohl (or van Laar) equation plot of the data, i.e., the form of Eq. (2), is closest to being linear, and therefore should be the better of the two-constant fits of the data. The data can, however, be fit quite well with a 3-constant Redlich-Kister expansion—See Illustration 10.1-4]



#Problem 4:
9.30

a)

$$i := 0, 1.. 10 \quad x_i := 0.1 \cdot i$$

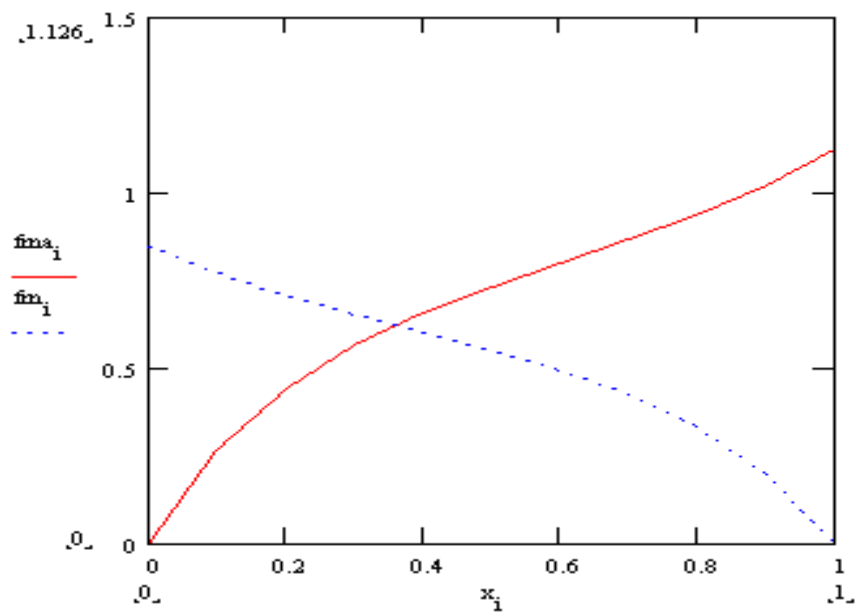
$$fma_i := x_i \cdot \exp[1.06 \cdot (1 - x_i)^2] \cdot 1.126$$

$$fm_i := (1 - x_i) \cdot \exp[1.06 \cdot (x_i)^2] \cdot 0.847$$

	0
0	0
1	0.1
2	0.2
3	0.3
4	0.4
5	0.5
6	0.6
7	0.7
8	0.8
9	0.9
10	1

	0
0	0
1	0.266
2	0.444
3	0.568
4	0.66
5	0.734
6	0.8
7	0.867
8	0.94
9	1.024
10	1.126

	0
0	0.847
1	0.77
2	0.707
3	0.652
4	0.602
5	0.552
6	0.496
7	0.427
8	0.334
9	0.2
10	0



b) from equation (9.7-12), we have

$$H_1 = \gamma_1(T, P, x_1 = 0) f_1^L = \exp\left[\frac{A}{RT} (1 - x_1)^2\right] * 1.126 = \exp(1.06) * 1.126 \quad (x_1 \rightarrow 0)$$

$$H_2 = \gamma_2(T, P, x_2 = 0) f_2^L = \exp\left[\frac{A}{RT} (x_1)^2\right] * 0.847 = \exp(1.06) * 0.847 \quad (x_2 \rightarrow 0)$$

Because of this, the hypothetical pure component fugacity based on the Henry's law standard state for methyl acetate and methanol would be, respectively:

$$\exp(1.06) * 1.126 = 3.25$$

$$\exp(1.06) * 0.847 = 2.445$$

which are different from values obtained from the usual pure component standard state

#Problem 5:

Consider an equimolar binary mixture of species a and b. The activity coefficients at infinite dilution are given by $\gamma_1^\infty (x_2 \approx 1) = 2$ and $\gamma_2^\infty (x_1 \approx 1) = 1.5$, calculate the activity coefficient of species a and b using the two-constant Margules expansion, Van Laar equation, and the Wilson equation

Solution

❖ Two-constant Margules expansion

$$RT \ln \gamma_1^\infty = (A + 3B) - 4B = A - B$$

$$RT \ln \gamma_2^\infty = (A - 3B) + 4B = A + B$$

$$\text{with } \gamma_1^\infty (x_2 \approx 1) = 2 \text{ and } \gamma_2^\infty (x_1 \approx 1) = 1.5$$

plug back into above equations, we obtain

$$A = RT \ln \sqrt{3}$$

$$B = RT \ln \frac{\sqrt{3}}{2}$$

For an equimolar mixture

$$RT \ln \gamma_1 = (A + 3B)(0.5)^2 - 4B * (0.5)^3$$

$$RT \ln \gamma_2 = (A - 3B)(0.5)^2 + 4B * (0.5)^3$$

Substitute the values of A and B into the above equations, we find

$$\gamma_1 = 1.11$$

$$\gamma_2 = 1.19$$

❖ Van Laar equation

$$\ln \gamma_1^\infty = \alpha = \ln(2)$$

$$\ln \gamma_2^\infty = \beta = \ln(1.5)$$

at equimolar mixture, we have

$$\ln \gamma_1 = \frac{\alpha}{\left[1 + \frac{\alpha}{\beta}\right]^2} = \frac{\ln 2}{\left[1 + \frac{\ln 2}{\ln 1.5}\right]^2}$$

$$\gamma_1 = 1.1$$

Similarly we have

$$\ln \gamma_2 = \frac{\beta}{\left[1 + \frac{\beta}{\alpha}\right]^2} = \frac{\ln 1.5}{\left[1 + \frac{\ln 1.5}{\ln 2}\right]^2}$$

$$\gamma_2 = 1.18$$

❖ Wilson equation

$$\ln \gamma_1^\infty = -\ln \Lambda_{12} + 1 - \Lambda_{21} = \ln 2$$

$$\ln \gamma_2^\infty = -\ln \Lambda_{21} - \Lambda_{12} + 1 = \ln(1.5)$$

Solving these two equations, we obtain

$$\Lambda_{12} = 0.407$$

$$\Lambda_{21} = 1.21$$

For an equimolar mixture

$$\ln \gamma_1 = -\ln(0.5 + 0.5\Lambda_{12}) + 0.5 \left[\frac{\Lambda_{12}}{0.5 + 0.5 * \Lambda_{12}} - \frac{\Lambda_{21}}{0.5 * \Lambda_{21} + 0.5} \right]$$

$$\ln \gamma_2 = -\ln(0.5 + 0.5\Lambda_{21}) - 0.5 \left[\frac{\Lambda_{12}}{0.5 + 0.5 * \Lambda_{12}} - \frac{\Lambda_{21}}{0.5 * \Lambda_{21} + 0.5} \right]$$

Solving the equations to get

$$\gamma_1 = 1.1$$

$$\gamma_2 = 1.17$$

#Problem 6:

The activity coefficients at infinite dilution of a binary mixture are given as $\gamma_1^\infty (x_2 \approx 1) = 1.27$, $\gamma_2^\infty (x_1 \approx 1) = 1.34$; calculate the activity coefficient of species 1 in the mixture, using one-constant Margules equation, at the following compositions $x_1 = 20\%$; $x_1 = 50\%$; $x_1 = 90\%$

Solution

With the one-constant Margules equation, we have

$$RT \ln \gamma_1^\infty = A = RT \ln(1.27)$$

$$RT \ln \gamma_2^\infty = A = RT \ln(1.34)$$

The value of A would be taken as the average, which is

$$A = 0.5 * RT * [\ln(1.27) + \ln(1.34)] = 0.266RT$$

At $x_1 = 20\% \rightarrow x_2 = 80\%$

$$RT \ln \gamma_1 = (0.8)^2 * A = 0.64 * 0.266RT$$

$$\gamma_1 = 1.186$$

At $x_1 = 50\% \rightarrow x_2 = 50\%$

$$RT \ln \gamma_1 = (0.5)^2 * A = 0.25 * 0.266RT$$

$$\gamma_1 = 1.069$$

At $x_1 = 90\% \rightarrow x_2 = 10\%$

$$RT \ln \gamma_1 = (0.1)^2 * A = 0.01 * 0.266RT$$

$$\gamma_1 = 1.003$$